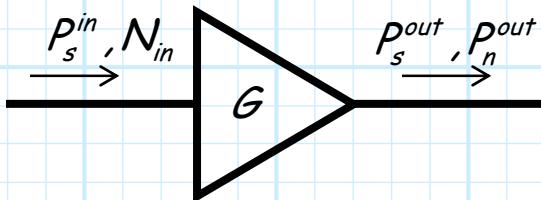


# Noise Figure and SNR

Of course, in addition to noise, the input to an amplifier in a receiver will typically include our desired signal.

Say the **power** of this input signal is  $P_s^{in}$ . The output of the amplifier will therefore include **both** a signal with power  $P_s^{out}$ , and noise with power  $P_n^{out}$ :



where:

$$P_s^{out} = G P_s^{in}$$

and:

$$\begin{aligned} P_n^{out} &= N_{in} + G k T_e B \\ &= G k (T_{in} + T_e) B \end{aligned}$$

In order to accurately demodulate the signal, it is important that signal power be **large** in comparison to the noise power. Thus, a fundamental and important measure in radio systems is the **Signal-to-Noise Ratio (SNR)**:

$$SNR \doteq \frac{P_s}{P_n}$$

The larger the SNR, the better!

At the output of the amplifier, the SNR is:

$$\begin{aligned} SNR_{out} &= \frac{P_s^{out}}{P_n^{out}} \\ &= \frac{GP_s^{in}}{Gk(T_{in} + T_e)B} \\ &= \frac{P_s^{in}}{k(T_{in} + T_e)B} \end{aligned}$$

Moreover, we can define an input noise power as the total noise power across the bandwidth of the amplifier:

$$P_n^{in} = N_{in} B = kT_{in} B$$

And thus the input SNR as:

$$SNR_{in} = \frac{P_s^{in}}{P_n^{in}} = \frac{P_s^{in}}{kT_{in}B}$$

Now, let's take the ratio of the input SNR to the output SNR:

$$\begin{aligned} \frac{SNR_{in}}{SNR_{out}} &= \frac{P_s^{in}}{kT_{in}B} \left( \frac{k(T_{in} + T_e)B}{P_s^{in}} \right) \\ &= \frac{T_{in} + T_e}{T_{in}} \\ &= 1 + \frac{T_e}{T_{in}} \end{aligned}$$

Since  $T_e > 0$ , it is evident that:

$$\frac{SNR_{in}}{SNR_{out}} = 1 + \frac{T_e}{T_{in}} > 1$$

In other words, the SNR at the **output** of the amplifier will be less than the SNR at the **input**.

→ This is very **bad news!**

This result means that the SNR will always be **degraded** as the signal passes through **any microwave component**!

As a result, the SNR at the **input** of a receiver will be the largest value it will **ever** be within the receiver. As the signal passes through each component of the receiver, the SNR will get steadily **worse**!

**Q:** Why is that? After all, if we have several amplifiers in our receiver, the signal power will significantly increase?

**A:** True! But remember, this gain will likewise increase the receiver input **noise** by the **same** amount. Moreover, each component will add **even more noise**—the internal noise produced by each receiver component.

Thus, the power of a signal traveling through a receiver increases—but the noise power increases even more!

Note that the ratio  $SNR_{in}/SNR_{out}$  essentially quantifies the degradation of SNR by an amplifier—a ratio of one is ideal, a large ratio is very bad.

So, let's go back and look again at ratio  $SNR_{in}/SNR_{out}$ :

$$\frac{SNR_{in}}{SNR_{out}} = 1 + \frac{T_e}{T_{in}}$$

Note what this ratio depends on, and what it does not.

This ratio depends on:

1.  $T_e$  (a device parameter)
2.  $T_{in}$  (**not** a device parameter)

This ratio does not depend on:

1. The amplifier gain  $G$ .
2. The amplifier bandwidth  $B$ .

We thus might be tempted to use the ratio  $SNR_{in}/SNR_{out}$  as another **device parameter** for describing the **noise** performance of an amplifier. After all,  $SNR_{in}/SNR_{out}$  depends

on  $T_e$ , but does **not** depend on other device parameters such as  $G$  or  $B$ .

Moreover, SNR is a value that can generally be easily measured!

But the problem is the **input** noise temperature  $T_{in}$ . This can be **any** value—it is **independent** of the amplifier itself.

For **example**, it is even that as the input noise increases to infinity:

$$\lim_{T_{in} \rightarrow \infty} \frac{SNR_{in}}{SNR_{out}} = \lim_{T_{in} \rightarrow \infty} \left( 1 + \frac{T_e}{T_{in}} \right) = 1$$

In other words, if the input noise is large enough, the internally generated amplifier noise will become **insignificant**, and thus will degrade the SNR **very little**!

**Q:** Degrade the SNR very little! This means  $SNR_{out} = SNR_{in}$ !  
Isn't this desirable?

**A:** Not in this instance. Note that if  $T_{in}$  increases to infinity, then:

$$\lim_{T_{in} \rightarrow \infty} SNR_{in} = \lim_{T_{in} \rightarrow \infty} \left( \frac{P_s^{in}}{kT_{in}B} \right) = 0$$

In other words, the SNR does not degrade by the amplifier **only** because the SNR is already as bad (i.e.,  $SNR = 0$ ) as it can possibly get!

Conversely, as the input noise temperature decreases toward zero, we find:

$$\lim_{T_{in} \rightarrow 0} \frac{SNR_{in}}{SNR_{out}} = \lim_{T_{in} \rightarrow 0} \left( 1 + \frac{T_e}{T_{in}} \right) = \infty$$

**Q:** Yikes! The amplifier degrades the SNR by an infinite percentage! Isn't this undesirable?

**A:** Not in this instance. Note that if  $T_{in}$  decreases to zero, then:

$$\lim_{T_{in} \rightarrow 0} SNR_{in} = \lim_{T_{in} \rightarrow 0} \left( \frac{P_s^{in}}{kT_{in}B} \right) = \infty$$

Note this is the **perfect** SNR, and thus the ratio  $SNR_{in}/SNR_{out}$  will likewise be infinity, **regardless** of the amplifier.

Anyway, the **point** here is that although the degradation of SNR by the amplifier does depend on the **amplifier** noise characteristics (i.e.,  $T_e$ ), it **also** on the noise input to the amplifier (i.e.,  $T_{in}$ ).

This input noise is a variable that is unrelated to amplifier performance

**Q:** So there is no way to use  $SNR_{in}/SNR_{out}$  as a device parameter?

**A:** Actually there is! In fact, it is the most **prevalent** parameter for specifying microwave device noise performance. This measure is called **noise figure**.

The noise figure of a device is simply the measured ratio  $SNR_{in}/SNR_{out}$  exhibited by a device, **for a specific input noise temperature  $T_{in}$** .

I repeat:

→ "for a specific input noise temperature  $T_{in}$ ."

This specific noise temperature is almost **always** taken as the standard "room temperature" of  $T_o = 290 K^\circ$ . Note this was likewise the standard **antenna noise temperature** assumption.

Thus, the **Noise Figure ( $F$ )** of a device is defined as:

$$\begin{aligned} F &\doteq \left. \frac{SNR_{in}}{SNR_{out}} \right|_{T_{in}=290K^\circ} \\ &= \left. \left( 1 + \frac{T_e}{T_{in}} \right) \right|_{T_{in}=290K^\circ} \\ &= 1 + \frac{T_e}{290K^\circ} \end{aligned}$$



It is critically important that **you** understand the definition of noise figure. A common **mistake** is to assume that:

$$SNR_{out} = \frac{SNR_{in}}{F} \quad \leftarrow \text{This is not generally true!}$$

Note this would only be true if  $T_{in} = 290K^\circ$ , but this is almost never the case (i.e.,  $T_{in} \neq 290K^\circ$  generally speaking).

Thus, an **incorrect** (but widely repeated) statement would be:



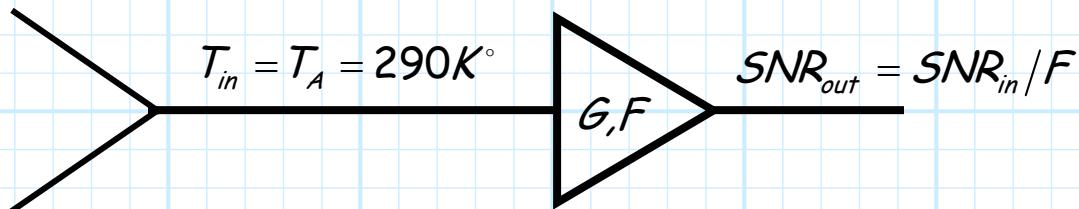
*"The noise figure specifies the degradation of SNR."*

Whereas, a **correct** statement is:



*"The noise figure specifies the degradation of SNR, for the specific condition when  $T_{in} = 290K^\circ$ , and for that specific condition only"*

The one **exception** to this is when an **antenna** is connected to the input of an amplifier. For this case, it is evident that the input temperature is  $T_A = T_{in} = 290K^\circ$ :



Note that since the noise figure  $F$  of a given device is dependent on its equivalent noise temperature  $T_e$ , we can determine the equivalent noise temperature  $T_e$  of a device with knowledge  $F$ :

$$F = 1 + \frac{T_e}{290K^\circ} \quad \Leftrightarrow \quad T_e = (F - 1)290K^\circ$$

One more point. Note that noise figure  $F$  is a unitless value (just like gain!). As such, we can easily express it in terms of decibels (just like gain!):

$$F(dB) = 10 \log_{10} F$$

Like gain, the noise figure of an amplifier is typically expressed in dB.